

Enhanced Faraday rotation via resonant tunnelling in tri-layers containing magneto-optical metals

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Abstract

We study resonant tunnelling effects that can occur in trilayer structures featuring a dielectric layer sandwiched between two magneto-optical(MO)-metal layers. We show that the resonance splitting associated with these phenomena can be exploited to enhance Faraday rotation at optical frequencies. Our results indicate that, in the presence of realistic loss levels, a tri-layer structure of subwavelength thickness is capable of yielding sensible ($\sim 10^\circ$) Faraday rotation with transmittance levels that are an order of magnitude larger than those attainable with a standalone slab of MO metal of the same thickness.

Keywords: magneto-optical effect, tunnelling, resonance, Faraday rotation

(Some figures may appear in colour only in the online journal)

1. Introduction

Faraday rotation effect (FRE), i.e. the rotation of the plane of polarization of a linearly-polarized electromagnetic wave propagating in a gyrotropic medium, is one of the most basic magneto-optical (MO) interactions [1], and finds important applications to realize nonreciprocal devices such as isolators and circulators. In essence, this effect relies on the *circular birefringence* of MO materials, for which circularly-polarized (CP) waves of opposite handedness (in terms of which a linearly-polarized wave can be decomposed) travel with different phase velocities.

At optical frequencies, typical MO materials (such as bismuth iron garnet [2, 3]) exhibit a rather weak gyrotropic response. Nonetheless, significant response enhancements can be obtained via artificial microstructures such as magneto-photonic crystals in the form of multilayers combining dielectric and MO materials [4–12], magneto-plasmonic devices [13–15], or epsilon-near-zero metamaterials [16].

On the other hand, MO metals such as $\text{Co}_6\text{Ag}_{94}$ [17] exhibit much stronger gyrotropic responses but, due to their

inherent opaqueness, are limited by very low transmission levels. However, two recent studies [18, 19] have shown the possibility to overcome this limitation (i.e. to significantly enhance the transmission) by pairing a thin MO-metal layer with an all-dielectric photonic or magneto-photonic crystal. From the physical viewpoint, this approach relies on resonant tunnelling effects that can occur in heterostructures containing *epsilon-negative* (ENG) and *mu-negative* (MNG) media [20–22]. More specifically, at optical frequencies, MO metals naturally behave as circularly-birefringent ENG media, whereas an all-dielectric photonic crystal operating in the bandgap region can effectively mimic an MNG-type behaviour [23]. Overall, taking into account realistic losses, multilayers containing a dozen layers (with total thickness of about 1.5 wavelengths) were shown to provide Faraday rotation angles of $\sim 15^\circ$, with transmittance levels ~ 0.3 that are about an order of magnitude higher than those pertaining to a standalone MO-metal slab [18, 19].

In this paper, we show that similar effects and comparable performance can be obtained with a simpler and more compact structure. Our approach is inspired by a series of studies

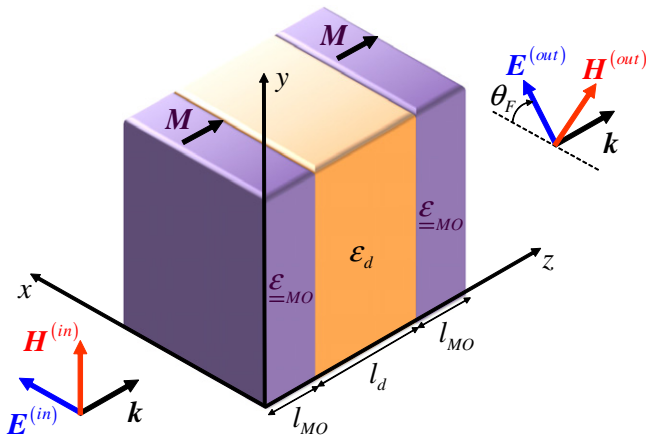


Figure 1. Problem schematic: a tri-layer structure (stacked along the z direction, of infinite extent in the x, y plane, and immersed in vacuum) composed of a dielectric layer of thickness l_d and relative permittivity ϵ_d sandwiched between two identical layers of MO-metal layers of thickness l_{MO} and relative permittivity tensor $\underline{\epsilon}_{MO}$ (assuming a static bias magnetization along the z -direction, see (1)). The structure is illuminated by a time-harmonic, linearly-polarized, normally-incident plane wave, with x -directed electric field. Ideally, the transmitted field is still linearly polarized, but with a rotation of an angle θ_F (Faraday rotation angle) of the plane of polarization.

on tunnelling effects occurring in heterostructures combining ENG and *double-positive* (i.e. with positive permittivity and permeability) material layers [24–32]. In particular, we consider a tri-layer structure of subwavelength thickness (~ 0.3 wavelengths) combining MO-metal and dielectric layers.

The rest of the paper is organized as follows. In section 2, we introduce the problem geometry and formulation, and outline the physical intuition as well as the main analytical derivations. In section 3, we present some numerical results in order to illustrate the FRE enhancement and quantitatively assess the performance, taking also into account realistic loss and dispersion effects. Finally, in section 4, we provide some concluding remarks and hints for future research.

2. Tunnelling and enhanced FRE in tri-Layers containing MO metals

2.1. Problem geometry and formulation

Referring to the geometry depicted in figure 1, we consider a tri-layer structure (stacked along the z -axis, of infinite extent in the x, y plane, and immersed in vacuum) composed of a dielectric layer of thickness l_d and relative permittivity ϵ_d sandwiched between two identical MO-metal layers of thickness l_{MO} . In the time-harmonic [$\exp(-i\omega t)$] regime, and in the presence of a static bias magnetization oriented along the z direction, such material is characterized by a gyrotropic relative permittivity tensor [33]

$$\underline{\epsilon}_{MO} = \begin{bmatrix} \epsilon_1 & -i\epsilon_2 & 0 \\ i\epsilon_2 & \epsilon_1 & 0 \\ 0 & 0 & \epsilon_3 \end{bmatrix}. \quad (1)$$

We assume that all materials are nonmagnetic and, for the moment, we neglect losses. At optical frequencies, the MO metal described by (1) is characterized by

$$\epsilon_1 < 0, \quad 0 < \epsilon_2 \ll |\epsilon_1|, \quad (2)$$

with ϵ_3 being irrelevant for our purposes. We consider the so-called Faraday configuration [33], by assuming a normally-incident linearly-polarized wave, with wavevector parallel to the static bias magnetization, and x -directed unit-amplitude electric field

$$\mathbf{E}^{(in)}(z) = \exp(ikz) \hat{x}, \quad (3)$$

where $k = \omega/c = 2\pi/\lambda$ denotes the vacuum wavenumber (and c and λ the corresponding wavespeed and wavelength, respectively), boldface symbols identify vector quantities, and the caret $\hat{}$ tags unit vectors. Our study is aimed at determining the conditions under which the impinging wave is significantly transmitted (with low reflection) through the structure, preserving its linearly-polarized character but with a rotation of an angle θ_F (Faraday rotation angle [34]) in the polarization plane (see figure 1).

2.2. Modelling and physical intuition

In the assumed conditions, the wave propagation in the MO metal is most naturally described in terms of *evanescent* (forward and backward) right-handed and left-handed CP (RCP and LCP, respectively) eigenwaves with electric fields [33]

$$\mathbf{E}_{RCP}^{(FW)}(z) = \exp(-\alpha_{(+)}z) (\hat{x} + i\hat{y}), \quad (4a)$$

$$\mathbf{E}_{RCP}^{(BW)}(z) = \exp(\alpha_{(-)}z) (\hat{x} - i\hat{y}), \quad (4b)$$

$$\mathbf{E}_{LCP}^{(FW)}(z) = \exp(-\alpha_{(-)}z) (\hat{x} - i\hat{y}), \quad (4c)$$

$$\mathbf{E}_{LCP}^{(BW)}(z) = \exp(\alpha_{(+)}z) (\hat{x} + i\hat{y}), \quad (4d)$$

where

$$\alpha_{(+)} = k\sqrt{-\epsilon_1 + \epsilon_2}, \quad \alpha_{(-)} = k\sqrt{-\epsilon_1 - \epsilon_2}, \quad (5)$$

denote the (real valued, in view of (2)) attenuation constants, which depend on the CP handedness and propagation direction. It is therefore expedient to decompose the linearly-polarized incident field in (3) in terms of RCP and LCP components,

$$\mathbf{E}^{(in)}(z) = \mathbf{E}_{RCP}^{(in)}(z) + \mathbf{E}_{LCP}^{(in)}(z), \quad (6)$$

with

$$\mathbf{E}_{RCP,LCP}^{(in)}(z) = \exp(ikz) \left(\frac{\hat{x} \pm i\hat{y}}{2} \right), \quad (7)$$

and invoke the superposition principle in order to reduce to a better problem-matched CP illumination. As anticipated, FRE is essentially based on the different phase velocities (and hence different phase accumulations) of RCP and LCP waves travelling in an MO material. However, given the evanescent character of the eigenwaves in (4a)–(4d), it is fairly evident that a standalone MO-metal slab would be *essentially opaque*. To give an idea, assuming $\epsilon_1 = -10.51$ and $\epsilon_2 = 1.15$ (realistic

values, aside for losses, at $\lambda = 631$ nm [17]), a standalone MO-metal slab of thickness 0.1λ would yield a transmittance as low as 0.023.

From the studies in [22], it is known that the opaqueness of an isotropic ENG slab can be ‘compensated’ by pairing it with a suitably matched MNG slab. Although these results may be readily extended to our gyrotropic case here, synthesizing MNG materials at optical frequencies is a very challenging task from the technological viewpoint. As a possible surrogate, the use of an all-dielectric photonic crystal or a magneto-photonic crystal operating in the bandgap was suggested in [18, 19], respectively.

There are, however, other ways to compensate an ENG slab by means of simpler, more compact, and yet nonmagnetic, structures, based, e.g. on the studies in [24–32]. The tri-layer structure in figure 1 is inspired by the isotropic ENG–dielectric–ENG tri-layer considered in [31], for which resonant tunnelling (with perfect transmission, in the absence of losses) was demonstrated. Extensions of such isotropic structure to the gyrotropic case were considered in [35, 36], by substituting the central dielectric layer with an MO material, thereby achieving one-directional tunnelling of CP waves. Here, instead, we substitute the two ENG layers with MO-metal ones, and derive the resonant tunnelling conditions for RCP and LCP waves. Contrary to the studies in [35, 36], we are not interested in achieving strong sensitivity of the tunnelling phenomena with respect to the CP handedness, but rather to attain high transmission of *both* RCP and LCP components in (6), so as to preserve the linearly-polarized character of the impinging field.

2.3. Analytical results and tunnelling conditions

Assuming an RCP or LCP excitation, the electromagnetic response of the tri-layer structure in figure 1 can be computed analytically in a rather straightforward fashion. Referring to appendix A for details, the transmission and reflection coefficients for RCP excitation (T_{RCP} and R_{RCP} , respectively) can be written as

$$T_{\text{RCP}} = \frac{2ikk_d\alpha_{(+)}^2 \operatorname{sech}(\alpha_{(+)}l_{\text{MO}}) \sec(k_d l_d)}{D_{\text{R}}}, \quad (8a)$$

$$D_{\text{R}} = \tau_d \left[\alpha_{(+)}^2 (\alpha_{(+)}\tau_{(+)} - ik)^2 - k_d^2 (\alpha_{(+)} - ik\tau_{(+)})^2 \right] - 2k_d\alpha_{(+)} (k\tau_{(+)} + i\alpha_{(+)})(k + i\alpha_{(+)}\tau_{(+)}), \quad (8b)$$

$$R_{\text{RCP}} = \frac{N_{\text{RR}}}{D_{\text{R}}}, \quad (9a)$$

$$N_{\text{RR}} = \tau_d \left[\alpha_{(+)}^2 (k_d^2 - k^2) + (k^2 k_d^2 - \alpha_{(+)}^4) \tau_{(+)}^2 \right] - 2k_d\alpha_{(+)}\tau_{(+)}(k^2 + \alpha_{(+)}^2), \quad (9b)$$

where

$$k_d = k\sqrt{\varepsilon_d}, \quad \tau_d = \tan(k_d l_d), \quad (10)$$

$$\tau_{(+)} = \tanh(\alpha_{(+)}l_{\text{MO}}). \quad (11)$$

For the LCP case, results are formally analogous, by replacing $\alpha_{(+)}$ with $\alpha_{(-)}$, namely,

$$T_{\text{LCP}} = \frac{2ikk_d\alpha_{(-)}^2 \operatorname{sech}(\alpha_{(-)}l_{\text{MO}}) \sec(k_d l_d)}{D_{\text{L}}}, \quad (12a)$$

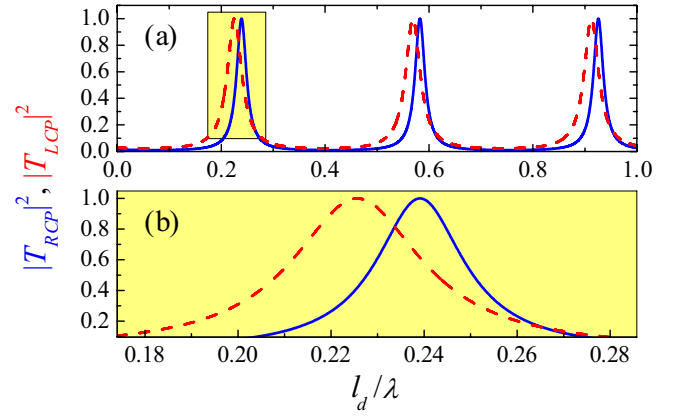


Figure 2. Geometry as in figure 1, with $\varepsilon_1 = -10.51$, $\varepsilon_2 = 1.15$, $l_{\text{MO}} = 0.05\lambda$, and $\varepsilon_d = 2.12$. (a) Transmittances of CP waves, $|T_{\text{RCP}}|^2$ (see (8a), blue-solid curves) and $|T_{\text{LCP}}|^2$ (see (12a), red-dashed curves), as a function of the dielectric layer electrical thickness. (b) Magnified detail around the lowest-order resonances, highlighting the resonance splitting.

$$D_{\text{L}} = \tau_d \left[\alpha_{(-)}^2 (\alpha_{(-)}\tau_{(-)} - ik)^2 - k_d^2 (\alpha_{(-)} - ik\tau_{(-)})^2 \right] - 2k_d\alpha_{(-)} (k\tau_{(-)} + i\alpha_{(-)})(k + i\alpha_{(-)}\tau_{(-)}), \quad (12b)$$

$$R_{\text{LCP}} = \frac{N_{\text{RL}}}{D_{\text{L}}}, \quad (13a)$$

$$N_{\text{RL}} = \tau_d \left[\alpha_{(-)}^2 (k_d^2 - k^2) + (k^2 k_d^2 - \alpha_{(-)}^4) \tau_{(-)}^2 \right] - 2k_d\alpha_{(-)}\tau_{(-)}(k^2 + \alpha_{(-)}^2), \quad (13b)$$

with

$$\tau_{(-)} = \tanh(\alpha_{(-)}l_{\text{MO}}). \quad (14)$$

From (9a) and (13a), the conditions for zero reflection (i.e. total transmission) for RCP and LCP excitation are readily derived as

$$l_d = \frac{1}{k_d} \arctan \left[\frac{2k_d\alpha_{(\pm)}\tau_{(\pm)}(k^2 + \alpha_{(\pm)}^2)}{\alpha_{(\pm)}^2(k_d^2 - k^2) + (k^2 k_d^2 - \alpha_{(\pm)}^4)\tau_{(\pm)}^2} \right], \quad (15)$$

where the (+) and (−) subscripts apply to RCP and LCP, respectively. In other words, for a given CP handedness, and assigned frequency and MO-metal layer parameters (l_{MO} , ε_1 , ε_2), it is *always* possible to find a dielectric layer of *arbitrary* relative permittivity ε_d and thickness l_d chosen according to (15) (plus its infinite half-wavelength periodicities) so that the power effectively tunnels through the tri-layer and is totally transmitted, despite the inherent opaqueness of the MO-metal constituents. We highlight that the guaranteed existence of a total-transmission solution as well as the completely arbitrary choice of the dielectric material make the tri-layer structure in figure 1 preferable to alternative tri-layer configurations such as, e.g. that in [24] (featuring an ENG layer sandwiched between two dielectric layers), or that in [28] (featuring an ENG layer paired at one side with a dielectric bilayer).

It is clear from (15) that, as a consequence of the aforementioned circular birefringence, the tunnelling conditions for the RCP and LCP excitations are *different*. Such *resonance-splitting* phenomenon is illustrated in figure 2,

which, for realistic parameters (aside for losses) of the MO-metal layer, shows the two transmittances as a function of the dielectric layer ($\epsilon_d = 2.12$) electrical thickness. As can be observed, the responses are characterized by a series of full-transmission peaks that are slightly shifted in the RCP and LCP cases. Therefore, in order to preserve the linearly-polarized character of the impinging field in (6), we cannot work at either of the RCP or LCP full-transmission peaks, but we rather need to settle to a *midway* condition for which

$$|T_{\text{RCP}}| = |T_{\text{LCP}}|. \quad (16)$$

For the assumed parameter configuration, this choice still allows a significantly high transmittance of ~ 0.8 (see the magnified details in figure 2(b)), i.e. ~ 35 times higher than that attainable in the presence of a standalone MO-metal slab of thickness $2l_{\text{MO}} = 0.1\lambda$. There is an evident tradeoff between the magnitude of attainable Faraday rotation, which benefits from a larger distance between transmission peaks for LCP and RCP waves, and the transmission level to achieve linearly-polarized output, which instead grows for smaller shifts.

3. Representative numerical results

3.1. Generalities and observables

The observables of interest in our study can be computed from the transmission and reflection coefficients in (8a)–(13b). In what follows, assuming the linearly-polarized excitation in (3), we compute the total transmittance (see (6)) as

$$|T|^2 = \frac{1}{2} (|T_{\text{RCP}}|^2 + |T_{\text{LCP}}|^2). \quad (17)$$

Moreover, for quantitative assessment of the FRE enhancement, we compute the Faraday rotation angle [34]

$$\theta_F = \frac{1}{2} \arctan \left(\frac{T_{\text{RCP}}}{T_{\text{LCP}}} \right). \quad (18)$$

Finally, to quantify the deviations from linear-polarization in the transmitted field, we compute the Faraday ellipticity [34]

$$\delta_F = \frac{|T_{\text{RCP}}| - |T_{\text{LCP}}|}{|T_{\text{RCP}}| + |T_{\text{LCP}}|}. \quad (19)$$

In the more realistic lossy case (see section 3.3), we also compute the total reflectance

$$|R|^2 = \frac{1}{2} (|R_{\text{RCP}}|^2 + |R_{\text{LCP}}|^2). \quad (20)$$

3.2. Ideal lossless case

We begin considering the ideal lossless case, by assuming the geometry and parameters as in figure 2. Figure 3 shows the three observables in (17)–(19) as a function of the dielectric layer electrical thickness. We can observe a series of equispaced, identical resonances characterized by high-transmittance peaks (figure 3(a)), accompanied by negative peaks in the Faraday rotation angle (figure 3(b)), and

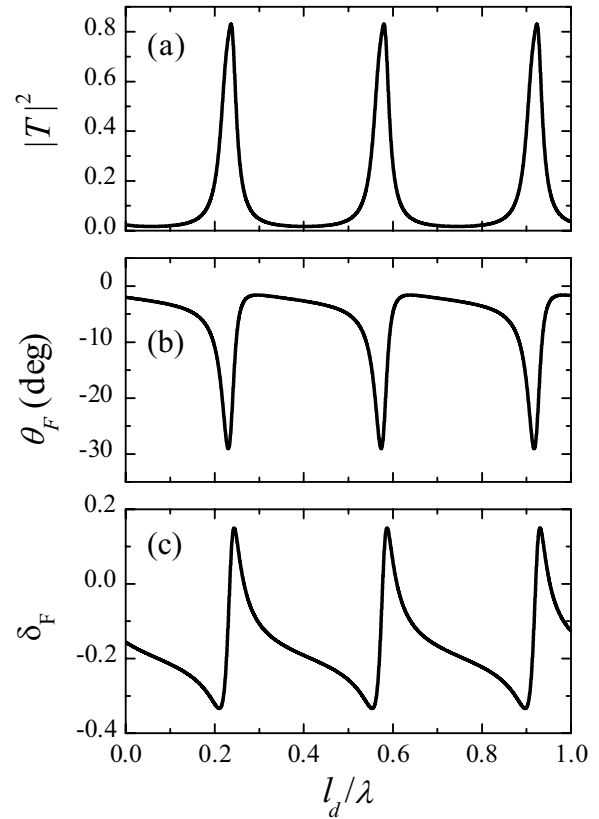


Figure 3. Parameters as in figure 2. (a) Total transmittance (see (17)), (b) Faraday rotation angle (see (18)), (c) Faraday ellipticity (see (19)), as a function of the dielectric layer electrical thickness.

abrupt variations (with zero crossing) of the Faraday ellipticity (figure 3(c)).

Next, we set the dielectric layer thickness to $l_d = 0.234\lambda$, so that the crossing condition in (16) is met at the operational wavelength (see figure 2(b)). This implies that, at that specific wavelength, the transmitted field will be linearly polarized. For instance, assuming (as in [18, 19]) a nominal operational wavelength $\lambda = 631$ nm (i.e. $l_d = 147$ nm), figure 4 shows the arising observables, as a function of the wavelength. It can be observed that, at the nominal operational wavelength, the Faraday ellipticity vanishes, thereby confirming the linear-polarization character of the transmitted field. This is accompanied by high transmittance (~ 0.8) and significant Faraday rotation angle ($\sim -28^\circ$), close to their peak values. To better understand the enhancement effects, it is worth recalling that a standalone MO-metal slab of thickness $2l_{\text{MO}} = 0.1\lambda$ would yield a transmittance $|T|^2 = 0.023$, a Faraday rotation angle $\theta_F = -2.02^\circ$, and a Faraday ellipticity $\delta_F = -0.157$.

Figure 5 shows the electric (solid) and magnetic (dashed) field-intensity distributions along the z -axis, inside and outside the tri-layer structure, at the nominal operational wavelength. Besides the high-transmission and low-reflection values already observable from figure 4, we notice a sensible field enhancement inside the tri-layer, with electric and magnetic fields peaked at the centre of the dielectric layer and at its boundaries with the MO-metal layers, respectively, accompanied by evanescent field growth in the left MO-metal

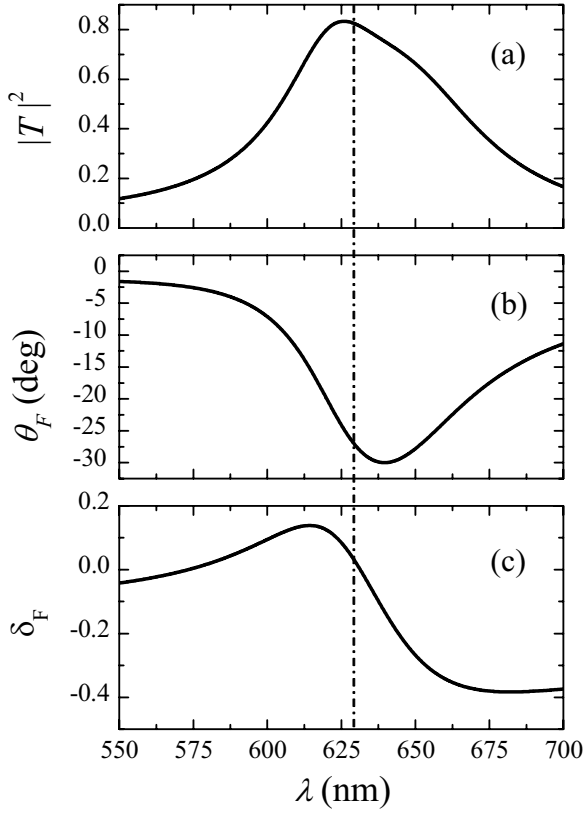


Figure 4. As in figure 3, but as a function of wavelength, assuming $l_{MO} = 32$ nm and $l_d = 147$ nm. The vertical dotted-dashed line indicates the nominal operational wavelength $\lambda = 631$ nm.

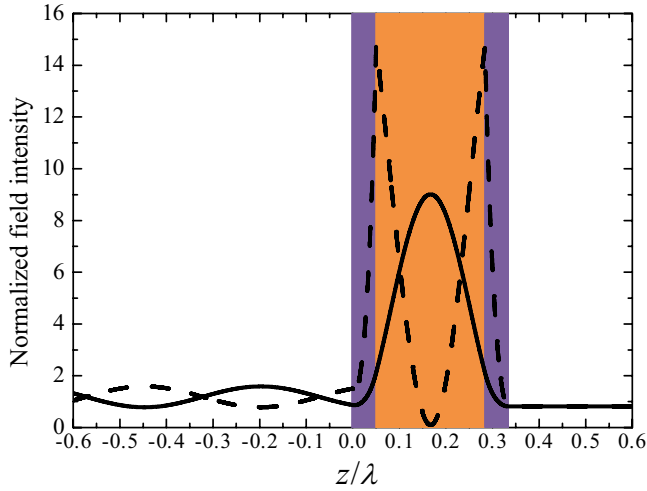


Figure 5. Parameters as in figure 4. Electric (solid) and magnetic (dashed) field-intensity distributions along the z axis (normalized by the incident field intensities, see (3)) at the nominal operational wavelength ($\lambda = 631$ nm). Different colours (consistent with figure 1) are used in order to visually delimit the various material layers.

layer. We note that the response resembles that of a Fabry–Pérot resonant cavity, with the end layers providing both the required high reflectivity and the MO activity.

3.3. Realistic lossy case

For a more realistic performance assessment, we need to take into account the inevitable loss and dispersion effects in the

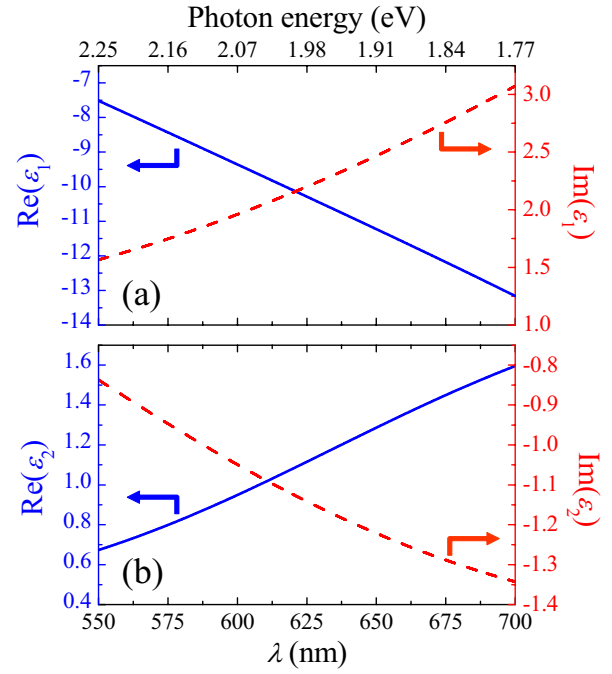


Figure 6. (a), (b) Dispersion laws for the real (blue-solid curves) and imaginary (red-dashed curves) parts of the relevant MO-metal relative permittivity components ϵ_1 and ϵ_2 , respectively, in (1). The curves are obtained by digitizing the experimental results in [17], pertaining to Co_6Ag_{94} measured at room temperature after annealing at $250^\circ C$.

MO-metal. Figure 6 shows the dispersion laws for the real and imaginary parts of the relevant constitutive parameters ϵ_1 and ϵ_2 in (1) obtained by digitizing the experimental results in [17], pertaining to Co_6Ag_{94} measured at room temperature after annealing at $250^\circ C$. For the dielectric layer, assuming fused silica (SiO_2) as a material, a lossless, nondispersive model with $\epsilon_d = 2.12$ can be safely adopted within the wavelength range of interest [37].

Figure 7 shows the same observables as in figure 4, but assuming now the MO-metal dispersion laws of figure 6. In addition, the reflectance $|R|^2$ in (20) is also shown (blue-dashed). Moreover, as a reference, also shown (red-dotted) are the corresponding observables pertaining to a standalone MO-metal slab of thickness $2d_{MO} = 64$ nm. By comparison with the ideal lossless case in figure 4, at the nominal operational wavelength $\lambda = 631$ nm, we note a sensible reduction of the transmittance ($|T|^2 \approx 0.3$, with reflectance $|R|^2 \approx 0.3$), which is, however, still over an order of magnitude higher than that achievable with a standalone MO-metal slab. Moreover, though reduced, the Faraday rotation angle ($\theta_F \approx -12^\circ$) is still enhanced by nearly a factor of three in comparison to the standalone MO-metal slab. Overall, the above results are in line with what observed in [18, 19], but our configuration is structurally simpler and more compact, its total thickness being only $\sim 0.3\lambda$ at the nominal operational wavelength. On the other hand, the Faraday ellipticity ($\delta_F \approx -0.35$), not considered in [18, 19], is nonnegligible.

It should be pointed out that our design procedure is based on the crossing condition of the split RCP and LCP resonances (see (16)) in the ideal lossless case. However, the

MO-metal losses affect the two CP polarizations in different ways. Therefore, in principle, better tradeoff configurations of the relevant observables may be found by taking into account the loss effects at the design stage. As an example, the contour plots in figure 8 show the three observables in (17)–(19), at the nominal operational wavelength, as a function of the MO-metal and dielectric layer thicknesses (l_{MO} and l_d , respectively) when MO-metal losses (see figure 6) are taken into account. From these plots, one may extract various tradeoff curves. For instance, for a targeted transmittance level, one may extract from figure 8(a) the iso-transmittance (l_{MO} , l_d) pairs, and derive from figures 8(b) and (c) a Faraday rotation angle versus ellipticity tradeoff curve. Figure 9 shows

three of such tradeoff curves (for targeted transmittance levels $|T|^2 = 0.2, 0.3$, and 0.4) where each point corresponds to a possible combination of the layer thicknesses l_{MO} and l_d extracted from figure 8. It can be observed that, by comparison with figure 7, tradeoff choices exist that, while maintaining comparable levels of transmittance ($|T|^2 \sim 0.3$) and Faraday rotation angle ($\theta_F \sim -10^\circ$), yield sensibly smaller ellipticities $\delta_F \sim -0.14$.

4. Conclusions and perspectives

In this paper, we have shown that enhanced FRE can be induced by resonant tunnelling in tri-layer structures featuring a dielectric layer sandwiched between MO-metal layers. Our analytical results allow for the derivation of simple design formulas, and provide a clear physical explanation of the phenomenon. In addition, we have assessed the performance in the presence of realistic loss and dispersion effects.

Overall, by comparison with alternative multilayered configurations [18, 19], we obtain comparable performance with a structurally simpler and thinner ($\sim 0.3\lambda$) configuration.

As possible follow-up studies, we plan to explore other nonreciprocal tunnelling phenomena inspired by the configurations in [24–32]. Also of interest are approaches to mitigating the effects of losses in the MO material constituents, e.g. along the lines of [38].

Appendix A. Derivation of (8a)–(13b)

Assuming a forward-propagating RCP excitation, we can express the electric field in the various regions of the structure in figure 1 as linear combinations of forward-propagating RCP waves and backward-propagating LCP waves, which are evanescent in the MO-metal layers, namely,

$$\mathbf{E}(z) = e(z) \frac{(\hat{x} + i\hat{y})}{2}, \quad (\text{A.1})$$

with

$$e(z) = \exp(ikz) + B_0 \exp(-ikz), \quad z < 0, \quad (\text{A.2})$$

$$e(z) = A_1 \exp(-\alpha_{(+)}z) + B_1 \exp(\alpha_{(+)}z), \quad 0 < z < l_{MO}, \quad (\text{A.3})$$

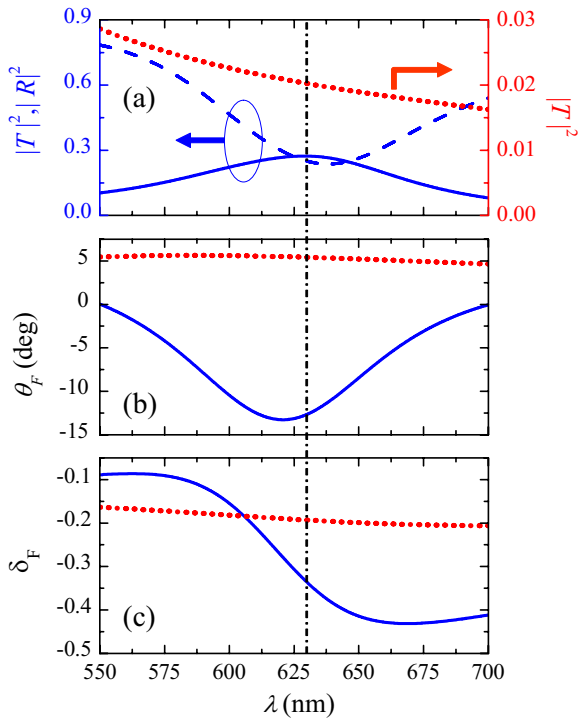


Figure 7. As in figure 5, but assuming the MO-metal dispersion laws in figure 6, and a lossless, nondispersive fused-silica (SiO_2) dielectric layer ($\epsilon_d = 2.12$). Also shown are the reflectance $|R|^2$ in (20) (blue-dashed curve) and the observables (red-dotted curves) pertaining to a standalone MO-metal slab of thickness $2l_{MO} = 64$ nm.

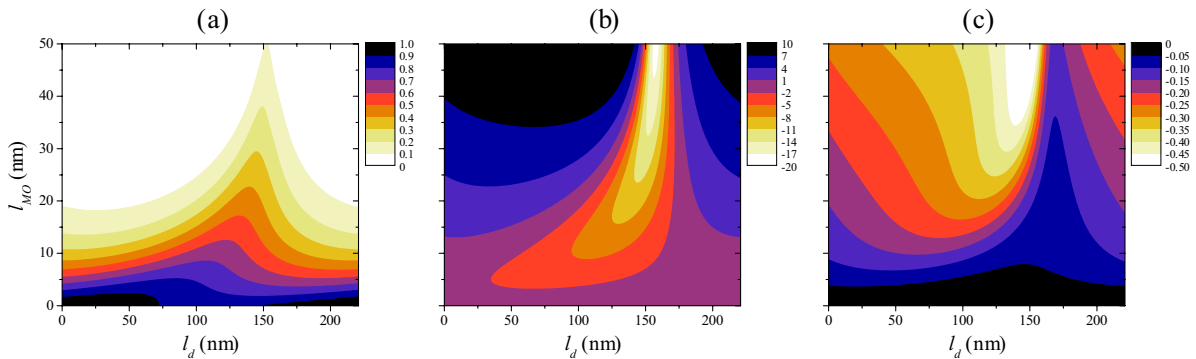


Figure 8. (a), (b), (c) Transmittance $|T|^2$, Faraday rotation angle θ_F (deg), and ellipticity δ_F , respectively, at the nominal design wavelength $\lambda = 631$ nm, as a function of the MO-metal and dielectric layer thicknesses. All other parameters are as in figure 7.

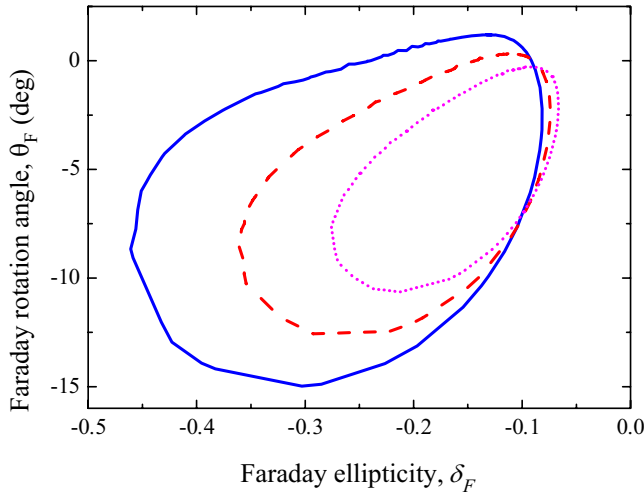


Figure 9. Tradeoff curves showing the Faraday rotation angle θ_F versus the ellipticity δ_F , at the nominal operational wavelength, for targeted transmittance levels $|T|^2 = 0.2, 0.3$ and 0.4 (blue-solid, red-dashed, and magenta-dotted curves, respectively). The curves are obtained by extracting the iso-transmittance (l_{MO}, l_d) pairs from figure 8(a), and the corresponding θ_F and δ_F from figures 8(b) and (c).

$$e(z) = A_2 \exp(ik_d z) + B_2 \exp(-ik_d z), \quad l_{MO} < z < l_{MO} + l_d, \quad (A.4)$$

$$e(z) = A_3 \exp(-\alpha_{(+)} z) + B_3 \exp(\alpha_{(+)} z), \quad l_{MO} + l_d < z < 2l_{MO} + l_d, \quad (A.5)$$

$$e(z) = A_4 \exp[ik(z - 2l_{MO} - l_d)], \quad z > 2l_{MO} + l_d. \quad (A.6)$$

The corresponding magnetic field can readily be derived from (A.1)–(A.6) via the relevant Maxwell’s curl equation

$$\mathbf{H}(z) = \frac{1}{i\omega\mu_0} \nabla \times \mathbf{E}(z), \quad (A.7)$$

with μ_0 denoting the vacuum permeability. Next, by enforcing the electric- and magnetic-field continuity at the four interfaces $z = 0, z = l_{MO}, z = l_{MO} + l_d$, and $z = 2l_{MO} + l_d$, we obtain an 8×8 linear system of equations whose (cumbersome but straightforward) solution yields the eight unknown coefficients $A_1, A_2, A_3, A_4, B_0, B_1, B_2$, and B_3 in (A.2)–(A.6). In particular, the transmission and reflection coefficients given in (8a)–(9b) are directly given by the coefficients A_4 and B_0 .

For the case of forward-propagating LCP excitation, the above procedure can be repeated in a formally analogous fashion, by assuming

$$\mathbf{E}(z) = e(z) \frac{(\hat{x} - i\hat{y})}{2}, \quad (A.8)$$

and replacing of $\alpha_{(+)}$ with $\alpha_{(-)}$ in (A.3) and (A.5). This yields the transmission and reflection coefficients in (12a)–(13b).

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